



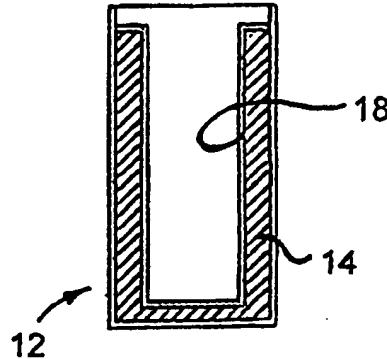
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(71) Applicant: EVEREADY BATTERY COMPANY, INC. [US/US]; 25225 Detroit Road, P.O. Box 450777, Westlake, OH 44145 (US).		
(72) Inventors: REICHERT, Samuel, Firestone; 259 Judita Drive, Brunswick, OH 44212 (US). CHANG, Bernice, Shou-Hua; 820 North Bay Drive P-16, Westlake, OH 44145 (US). KEOUGH, Kevin; 30 Sheffield Drive, Canton, MA 02021 (US). HARVEY, Andrew, C.; 60 Woodchester Road, Waltham, MA 02154 (US). KOVAR, Robert, Francis; 203 Beech Street, Waltham, MA 02093 (US). TIANO, Thomas, M.; 6 Pinewood Road, Hudson, NH 03051 (US).		Published <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>
(74) Agents: WELSH, Robert, W. et al.; Eveready Battery Company, Inc., 25225 Detroit Road, P.O. Box 450777, Westlake, OH 44145 (US).		

(54) Title: FORMED IN SITU SEPARATOR FOR A BATTERY

## (57) Abstract

A battery including a polar solvent transportive, ionically conductive separator formed directly on an electrode is prepared by applying a coating composition containing a polymer or gel dispersed in a polar solvent directly to the electrode surface and solidifying materials in the coating composition to form a separator membrane.



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FORMED IN SITU SEPARATOR FOR A BATTERY

This invention relates to batteries and in particular to separators for alkaline cell.

5        Alkaline batteries are generally cylindrical in shape and include an annular cathode disposed between the outer casing of the battery or can, and the anode material which occupies a cylindrical volume having a longitudinal axis generally coincident with that of the battery and can. Located between the cathode and the anode material is a separator which electrically insulates the cathode from the anode material, but which  
10      absorbs electrolyte and allows water transport and ion transfer between the electrodes. Heretofore, the separators used in alkaline batteries have generally been limited to commercially available battery separator papers and cellophane films.

15      While conventional battery separator paper has proven satisfactory, it would be desirable to provide methods and materials which would allow the separator to be installed at a lower cost using a simplified process and apparatus. In particular, the equipment used to cut and place the paper separators into the batteries is relatively complicated and expensive. Additionally, preparing the equipment used to cut and place the paper separators into the batteries requires sampling of the paper used to form  
20      the separators and adjustments of the equipment depending on the particular properties of the paper being used.

25      Another problem with the use of paper separators is that process reliability is sensitive to the internal diameter of the cathode. For example, variations in the internal diameter of the cathode along the longitudinal length of the battery can result in areas wherein the separator does not intimately contact the cathode. Also, changes in anode basket volume affect cell performance. As a result, the interfacial area for ionic transport may be substantially reduced as compared with a battery having a separator basket with an internal diameter which does not vary along either the longitudinal or  
30      radial direction and wherein the separator is substantially in continuous contact along the entire internal cylindrical surface of the cathode.

Another problem with paper separators is that because of the relatively complicated manipulations required to place the separators into the batteries, long process cycle times are required and process capability is generally low and varies widely between machines and even for any particular machine.

5

A still further disadvantage with paper separators is that the paper takes up a substantial amount of volume within the cell, which, in turn, requires a substantial amount of electrolyte to wet the separator. Paper separators work optimally when wet and less efficiently when only damp.

10

Also, the paper does not intimately contact the cathode over the entire cathode/separator interface, especially at the bottom of the separator where the folds occur, creating unused volume within the cell. Side seams of conventional paper separators also consume cell volume. A still further disadvantage with conventional paper separators is that the defect rate is greater than desired.

15

An alternative method for preparing an electrochemical cell which does not involve the use of a paper separator involves forming a polystyrene separator by placing a predetermined amount of polystyrene solution directly on the surface of a cathode and removing the organic solvent, thereby leaving a substantially continuous coating on the surface of the cathode. This method is generally undesirable and impractical because it typically requires placement of a reinforcing means on the surface of the cathode before application of the solution containing polystyrene, and requires evaporating large quantities of volatile organic solvents such as methylene chloride, tetrahydrofuran, ethyl acetate, acetone, benzene, toluene, and trichloroethylene. Placing of a reinforcing means on the surface of the cathode adds to the cost of the battery and requires complicated automation comparable to that required for automatically incorporating a paper separator into a battery. The use of volatile organic solvents is extremely undesirable due to health related issues (e.g., toxicity), safety related issues (e.g., flammability) as well as the difficulty and expense involved in avoiding environmental

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contamination. Some solvents, if not entirely removed, can detrimentally affect cell performance.

It would therefore be desirable to be able to provide an improved method of  
5 constructing a battery using a separator which is installed within the battery without  
folding operations, and elimination of the various problems enumerated above relating  
to the use of conventional paper separators and polystyrene separators. It would also be  
desirable to be able to provide batteries having improved volumetric efficiency,  
improved solvent transport characteristics across the separator, and improved ionic  
10 conductivity across the separator.

We have now found that the above objectives may be achieved, and the  
disadvantages with paper separators enumerated above may be overcome, by a battery  
having a separator formed directly on an electrode by applying a coating composition  
15 comprising a polymer or gel dispersed in a polar solvent to the surface of the electrode  
and solidifying materials in the applied coating composition.

Accordingly, in a first aspect, the present invention provides a battery  
comprising first and second electrodes, an alkaline electrolyte, and an ionically  
20 conductive separator disposed between the electrodes, the separator being formed by  
applying a coating composition to the surface of at least one of the electrodes and  
solidifying material contained in the coating composition, the coating composition  
comprising a gel or polymer dispersed in a polar solvent.

25 In a second aspect, the present invention provides a method of providing a  
separator on an electrode for an alkaline battery, comprising:  
applying a liquid aqueous coating composition to an electrode surface; and  
solidifying the coating composition on said electrode surface to form a separator  
membrane.

The present invention will be further understood by reference to the drawings, in which:

Figures 1-3 illustrate a method for forming a separator directly on a cathode by  
5 applying a coating composition to the cathode surface and allowing the coating  
composition to solidify; and

Figure 4 illustrates an alternative apparatus for applying a coating composition to  
a cathode surface of an alkaline battery.

10 The invention encompasses batteries having a separator which is formed directly  
on an electrode by applying a polar solvent based coating composition, such as an  
aqueous coating composition, to the electrode surface and allowing the coating  
composition to solidify. Although the invention will be primarily described with  
respect to cylindrical batteries, it is not limited to cylindrical shaped batteries, but  
15 instead may be applied to batteries of various other shapes.

The expression "polar solvent based coating composition" refers to a  
composition which can be applied to a surface using liquid coating techniques, and  
wherein the solvent portion of the composition is comprised mostly of polar molecules.

20 Examples of polar solvents include water, alcohol, and sulphuric acid. The invention  
hereinafter will, in general, be described with respect to aqueous coating compositions,  
it being understood that other polar solvents may be employed in accordance with the  
present invention.

25 The method involves using any of various conventional coating application  
techniques including, but not limited to, centrifugal casting, spinning disk coating, spray  
coating, slush moulding, electrostatic spraying and thermoforming. Other application  
techniques which may be used include inverted can spray coating wherein the coating  
composition is sprayed vertically upwardly into an inverted battery can containing a  
30 cathode, dip coating wherein the battery can containing the cathode is filled with the  
coating material and excess coating material is subsequently poured out of the battery

can, pad coating wherein an expendable cylindrical pad is dip coated with the coating composition and pressed against the inner surface of the cathode to transfer the coating composition to the cathode surface, brush coating, roll coating, slot extrusion coating wherein the coating composition is applied to the cathode surface from an extrusion die, 5 vacuum forming, blow moulding, and pour-in-place gelling wherein a gel precursor is poured into the cathode and a forming plug is thereafter inserted into the cathode followed by rapid curing, or a combination of these techniques. Presently preferred coating application techniques include ram moulding, centrifugal casting, and spray coating. Thus, the separator will preferably be in substantially continuous contact with 10 the surface of the electrode upon which it is formed.

The ram moulding technique for applying the coating composition to the internal surfaces of the cathode is illustrated in Figures 1-3. As shown in Figure 1, the coating composition 10 is introduced into the bottom of a battery 12 having a cathode 14. Next, 15 as shown in Figure 2, a forming ram 16 is introduced into the cathode to cause the coating composition to flow up between the ram and the inner surface of the cathode. After the coating composition solidifies or sets, the ram 16 is removed from the battery 12, leaving a separator 18 which is formed directly on the cathode.

20 In Figure 4, there is shown an alternative forming ram 20 having an internal conduit or bore 22 with an outlet port 24 at a lower end thereof. The forming ram 20 is first inserted into the battery 12 having a cathode 14 as shown in Figure 4. Thereafter, coating composition is introduced into the bottom of the battery through conduit 22 from outlet port 24. The coating composition flows through the ram, into the bottom of 25 the battery, and up into the annulus between the ram and the inner surface of the cathode 14.

The ram moulding technique is believed to have several potential advantages. First, the shape of the formed separator 18 can be controlled by controlling the 30 dimensions of the ram and the cathode internal diameter. Variations in temperature, viscosity, and solids loading in the liquid coating composition can be tolerated. This

allows refinements in the coating composition to be made without changing the application process. The ram design can allow the shape of the separator to be tailored to improve performance characteristics. For example, the edges of the ram can be chamfered to decrease stress risers in the separator membrane. Also, the thickness of  
5 the membrane can be varied at different locations. The ram geometry allows the coating composition to be accurately applied over the top of the cathode shelf 26, along the sides 28, and on the bottom surface of the can. The anode volume formed by ram moulding can be very accurately controlled as compared with conventional batteries having a folded paper separator. The ram moulding technique is well suited to  
10 continuous automated production.

Another desirable technique for applying the coating composition to the inner surface of the cathode is centrifugal casting or spin coating. This technique involves first introducing the coating composition into a cathode cup disposed in and integrally  
15 connected to a cylindrical can. Thereafter, the cathode cup and cylindrical can are rotated at a high speed, or may already be rotating at a high speed when the material is introduced. As the cathode rotates, the material flows up along the internal surface of the cathode and solidifies or cures in place. The axis of rotation of the cylindrical can in which the cathode is disposed may be at any angle between and including a vertical axis  
20 and a horizontal axis. The can may be inverted such that gravitational acceleration assists the flow of coating composition out of the can.

Centrifugal casting is believed to have several advantages including even coating of the internal cathode surface regardless of surface irregularities on the cathode surface,  
25 filling of voids in the cathode surface such as where the cathode material spalls off during cathode moulding, and the ability to provide fixed or predetermined separator material volume. The centrifugal casting technique is tolerant to loose particles of cathode material left from cathode moulding. Another advantage of centrifugal casting or spin coating is that the internal surface of the separator will be very smooth.  
30

Another desirable technique for applying the coating composition to the internal surface of the cathode is spray coating. With this technique, the liquid separator coating

composition is sprayed onto the surface of the cathode and solidifies or cures in place. A major advantage of the spray coating process is its mechanical simplicity.

The aqueous separator coating composition may be an aqueous solution, gel,  
5 dispersion, slurry, or combination thereof which can be applied in liquid form using liquid coating application techniques, and which will solidify to form a separator directly on the cathode surface. Solidification of the coating composition refers to any process of drying, curing, gelling, cross-linking, polymerisation, freezing (*i.e.*, thermal solidification), or combination thereof which results in a stable electrically insulating  
10 barrier which will allow ionic transport between the electrodes and will adhere to the cathode during the production and useful life of a battery.

The solidified coating is preferably less than 510 µm (0.020 inches) thick, more preferably less than 130 µm (0.005 inches), with thinner coatings being desirable to  
15 maximise anode basket volume. The separator coating compositions preferably smooth out or fill any surface irregularities in the cathode surface and preferably have controllable thickness, including uniform and variable thickness.

An advantage with the formed *in situ* separators is that they are in intimate and  
20 complete contact with the electrode surface on which they are formed, *i.e.*, the separator is in substantially continuous contact with the surface of the electrode upon which the separator is formed. This differs significantly from paper separators which normally have significant areas which are not in contact with adjacent electrode surfaces. The improved contact provided by the *in situ* formed separators provides enhanced ion  
25 transport properties and improved cell performance. The formed *in situ* separators can be made thinner than paper separators and can therefore occupy less space than a paper separator, thereby allowing more space in a battery for electrode material, and hence enabling improved battery performance. For example, the formed *in situ* separators may be employed to provide batteries in which the separator occupies less than 10% of the  
30 cell volume.

- The solidified or cured separators should be mechanically tough, resistant to mechanical shock and not easily ruptured or damaged once cured. The resulting separator should also exhibit sufficient tear resistance to prevent tears across gaps between the cathode rings, cathode-to-can interfaces, or the surfaces of the anode. The
- 5     separator coating composition should also solidify or cure to form a separator membrane having sufficient elasticity to sustain at least 25 % expansion of the cathode dimensions during discharge without tearing or separating from the electrode. The separator should also exhibit sufficient penetration resistance to resist penetration by zinc dendrites and should not provide a path for formation of zinc dendrites as do paper separators. The
- 10    compression strength of the separator should be sufficient to prevent squeeze-out of liquid under full compression between a discharged anode and cathode. The separator should retain efficient mechanical properties throughout the operating temperature range of -20°C to 71°C, but also -40° to 85°C abuse temperatures.
- 15    The separator should also exhibit high retentiveness of electrolyte solution, even under compression and when either the anode or cathode are dried out, *i.e.*, the separator should be the last component to dry out during cell discharge. The separator must remain dimensionally stable in the presence of 45 % potassium hydroxide, and should not swell or shrink in the presence of water or potassium hydroxide and retain
- 20    mechanical integrity. Further, the separators should preferably adhere to ring moulded, and impact moulded electrodes. The separators should also preferably adhere to rod-shaped, ring-shaped, strip-shaped, washer-shaped, and other shaped electrode surfaces.
- In addition to the above mechanical requirements, the separator should exhibit
- 25    certain electrical properties. First, the separator should not be electrically conductive, *i.e.*, it should act as an electrical insulator between the anode and cathode. The separator should maintain the electrical insulating characteristics over the projected life of the battery, which is at least about 5 years. The separator should also exhibit high ionic conductivity which meets or exceeds the hydroxyl ion flux density of the anode at
- 30    the anode/separator interface, and which meets or exceeds the hydroxyl ion flux density of the cathode at the cathode/separator interface, *i.e.*, the separator should not be rate

limiting. The separator should also have surface-to-surface ion conducting pathways, even in partially dehydrated condition.

The separator should also exhibit certain chemical properties. First, the  
5 separator must be chemically stable or inert (i.e., must not decompose) in a 45 % potassium hydroxide solution. The separator should also exhibit chemical stability under a potential difference of up to 2 volts. The separator should also exhibit high gas permeability. In order to prevent local conditions favourable to zinc oxide precipitation, the separator should exhibit good shorting resistance. The separator must not cause  
10 corrosion of nickel plated steel at the cathode potential, and should exhibit minimum permanent bonding of electrolyte and water. The separator should also be resistant to catalytic decomposition by the metals used in the construction of the battery.

Water and ionic transport properties are also an important consideration. Water  
15 should readily diffuse through the separator so that small concentration gradients will result in high diffusion rates. Poor diffusion would result in cell polarisation under heavy drain. The separator must pass hydroxyl ions from cathode to anode and must pass potassium ions from anode to cathode. The pathway for ion transport should be somewhat tortuous. A suitable transference number of hydroxyl ion in potassium  
20 hydroxide is 0.73. The hydration number of potassium ion should be from about 1 to about 2. The separator should act as a barrier to prevent movement of electrode materials from the cathode to anode and from the anode to the cathode. Desirably, the coating compositions should offer the ability to tailor the transport characteristics.

25 The coating compositions of this invention may solidify or freeze to form an aqueous gel separator having a solvent content greater than 50%, preferably greater than 90%, by weight. This high solvent content allows the separator to behave as an electrolyte reservoir.

30 It is believed that a wide variety of aqueous gels, and polymer dispersions can be formulated to achieve the desired separator characteristics. Examples of coating

compositions which have been found to be suitable for forming a separator directly on the surface of a cathode include seamless gels comprising kappa-carrageenan, hydroxyethyl cellulose, and a blend of kappa-carrageenan and hydroxyethyl cellulose. Other suitable compositions may include lambda- or iota-carrageenan, other 5 hydroxyalkyl celluloses such as hydroxymethyl- and/or hydroxypropyl cellulose, and combinations thereof. For example, kappa-carrageenan forms a strong film when cast as a 2-5 weight percent film with water. Hydroxyethyl cellulose cross-linked with vinyl sulphone forms a strong gel with very high ionic conductivity. However, separators formed from kappa-carrageenan alone are not as strong as would be desired, and 10 separators cast from hydroxyethyl cellulose alone exhibit shrinkage which is generally more than would be desired for AAA and larger size cells, but is acceptable for smaller cells. Other coating compositions which may be employed include aqueous compositions containing polyvinylpyrrolidone, such as compositions comprised of carrageenan (e.g., kappa-, lambda-, and/or iota-carrageenan) and polyvinylpyrrolidone.

15

It has been discovered that separator coating compositions containing a blend of kappa- carrageenan and hydroxyethyl cellulose are capable of forming separators exhibiting very high ionic conductivity with exceptional strength and shrinkage characteristics. Thus, a blend of two different polymers may be employed to provide a 20 composition which can be used to form *in situ* separators having an outstanding combination of properties.

Kappa-carrageenan is a naturally occurring marine colloid. More specifically, kappa-carrageenan is a sulphur phycocolloid (a polysaccharide) occurring in algae. A 25 major potential advantage of kappa-carrageenan as a separator is that it is a low-temperature thermoformable thermoplastic gel, preferably having a melting point greater than 71°C. Other potential advantages are that it is non-toxic, water-soluble, very low in cost, and readily available commercially. The separators may be cast from a coating composition containing approximately 1 to 10 percent, and more desirably 2 to 5 30 percent, by weight of the composition. However, higher and lower concentrations may be used.

Hydroxyethyl cellulose is a non-ionic, water-soluble, cellulose ether. The potential advantages of hydroxyethyl cellulose as a battery separator material are that it is water-soluble, low cost, commercially available, can be chemically cross-linked (with 5 divinylsulphone, for example) and is compatible with other aqueous based polymers. A suitable separator coating composition which can be used to form a battery separator may be prepared as a 5 weight percent mixture of hydroxyethyl cellulose in water, although higher and lower concentrations may also be used. Divinylsulphone cross-linking agent is desirably added to the coating composition in an amount of from about 10 0.05 to about 2% of the weight of the hydroxyethyl cellulose, and more desirably from about 0. 10 to about 1 weight percent. In general, higher amounts of cross-linking agent provide separators which exhibit higher electrical resistance and greater strength at the expense of ionic conductivity.

15 Another material which has been found suitable for preparing a separator directly on a cathode surface is cellulose viscose. Cellulose viscose is a viscous liquid consisting of concentrated aqueous alkali containing a solution of cellulose/xanthate complex. It can be coagulated in dilute (e.g., 10%) sulphuric acid to form regenerated cellulose. The potential advantages of cellulose viscose are that it is water-soluble, low 20 cost, stable to concentrated alkali, and has an existing performance record in alkaline batteries. Separators can be cast from solutions containing about 5 weight percent cellulose/xanthate complex, although higher and lower concentrations may also be used.

25 Examples of other materials which can be used in the preparation of the coating compositions which are applied to the cathode to form a separator include various synthetic polymers prepared as aqueous dispersions. Examples include aqueous dispersions of cellulose, polyurethane, acrylic polymers, polyvinyl acetate, and epoxy polymers; and dispersions of cellulose in polar organic solvents such as N-methyl morpholine oxide.

The coating compositions may and often desirably contain fibres, such as wood pulp, polyolefin, cellulose, cotton, rayon, boron, boron carbide, boron nitride, carbon, aluminium silicate, and/or fused silica fibres. Polyolefin fibres include halogenated polyolefin fibres, such as those prepared from fluorinated polypropylene. The amount of fibre in the composition is desirably from about 3 % to about 50 %, and more preferably from about 3 % to about 20%, of the weight of the polymer or gel material in the composition. Fibres are included to provide physical barrier integrity, and to reinforce and structurally strengthen the separator.

10       Particularly preferred coating compositions are those comprising kappa-carrageenan, hydroxyethyl cellulose, and cellulose fibres. The hydroxyethyl cellulose, kappa-carrageenan, and cellulose fibres are preferably dispersed in water to form the separator coating composition. The weight ratio of hydroxyethyl cellulose to kappa-carrageenan is preferably from about 1:3 to 3:1, and more preferably from about 1:1 to 15       about 3:1, although higher and lower ratios may also be used. The amount of hydroxyethyl cellulose and kappa-carrageenan in the coating composition may vary considerably, but is generally from about 1 % to about 10% by weight, although higher and lower concentrations may also be used.

20       Cross-linking agents such as divinylsulphone may be employed in amounts up to about 2% of the weight of the composition. Another suitable cross-linking agent which may be employed is trishydroxy methyl cyanurate, which is commercially available from American Cyanamid and sold under the trademark CYMEL®. The coating compositions preferably have a solvent content greater than 50% by weight during 25       application.

30       In a preferred embodiment, the coating composition is a polymer dispersion comprising hydroxyethyl cellulose in water and containing divinylsulphone cross-linking agent in an amount of from about 0.05 to about 2% of the weight of the composition.

In another preferred embodiment, the coating composition is a polymer dispersion comprising kappa-carrageenan, lambda-carrageenan, iota-carrageenan, hydroxymethyl cellulose, hydroxyethyl cellulose, hydroxypropyl cellulose, or a combination thereof.

5

In yet another preferred embodiment, the coating composition is comprised of kappa-carrageenan, hydroxyethyl cellulose, and divinylsulphone cross-linking agent, the weight ratio of hydroxyethyl cellulose to kappa-carrageenan is from about 1:3 to about 3:1, and the amount of cross-linking is from about 0.05 to about 2% of the weight of the composition. More preferably, the amount of hydroxyethyl cellulose and kappa-carrageenan in the coating composition is from about 1 % to about 10 % by weight. Preferably, this coating composition further contains an amount of fibre which is from about 3 % to about 50 % of the weight of the composition.

15

The present invention will now be described with reference to the following non-limiting examples:

## EXAMPLES

20 Fabrication Of Functional Batteries

Three master batches of separator coating compositions were prepared. The first coating composition contained 5 % by weight kappa-carrageenan in water. The second coating composition contained 5 weight percent hydroxyethyl cellulose in water with 1 weight percent potassium hydroxide. The third coating composition was a 3:1 mixture of the kappa-carrageenan master batch to the hydroxyethyl cellulose master batch. The kappa-carrageenan and kappa-carrageenan hydroxyethyl cellulose blends were heated above 90°C to melt the kappa-carrageenan and were held between 90°C and 100°C in a double boiler. A stainless steel ram was fabricated that was 1mm (40 mils) smaller in diameter than the inside diameter of a D cell cathode. The ram or mandrel was mounted in a collet on a vertical milling machine. A V-block was positioned on a machine table such that when a D cell was clamped in the V-block the centre line of the ram was in

line with the centre of the cell. A spindle stop on the machine was set so that the ram would stop approximately 1.6 mm (1/16 inch) above the bottom of the can. With this configuration, the formed separator was to be 0.5 mm (0.020 inches) thick on the cathode surface and 1.6 mm (0.062 inches) thick on the bottom. The separator could 5 actually be significantly thinner than this. However, during the developmental work it was preferable to have a thicker separator than needed, to compensate for example for any tooling inaccuracies, cathode particle entrapment, or bubbles in the liquid separator. Separators were formed from the kappa-carrageenan coating composition and from the kappa-carrageenan/hydroxyethyl cellulose blend in the cells by filling the cells to the top 10 with the liquid separator coating composition and lowering the ram into the cathode. As the ram entered the cathode, excess liquid flowed out. After the separator material cured or solidified, the ram was removed. In the case of the hydroxyethyl cellulose formulation, vinyl sulphone cross-linker was added and mixed prior to pouring the material into the cathodes. The filling and ram forming process was performed twice on 15 each cell in order to fill any voids that might be caused by for example air bubbles, or uneven separator material flow. Anode paste was added to fill the cells to the top of the cathode and collector assemblies were placed on the cells.

Nine cells were formed with the kappa-carrageenan separator material. All of 20 the cells had an initial voltage of from 1.51 to 1.64 volts. Seven functional cells were put on 71°C shelf-life testing. Two of the cells had an open circuit voltage (OCV) above 1.2 after storage for 5 weeks at 71°C.

Four cells were made using the kappa-carrageenan/hydroxyethyl cellulose blend. 25 Two of the cells had an initial voltage above 1.5. The other two cells have voltages below 1.2.

Based on these tests, it was determined that battery separator membranes made from kappa-carrageenan coating compositions and kappa-carrageenan/hydroxyethyl 30 cellulose coating compositions can be used in alkaline cells. These tests also

demonstrated that the ram moulding process for forming the separator membranes is workable.

Fabrication of AA Batteries

5       AA alkaline batteries were prepared as follows. A 5 weight percent solution of kappa-carrageenan in water was prepared. The kappa-carrageenan solution was held at 90°C in a hot water bath. A large syringe with a hypodermic needle was filled with the kappa-carrageenan solution. The kappa-carrageenan coating composition was introduced to the bottom of the AA can containing the cathode. The can containing the  
10      cathode was filled to the top with the kappa-carrageenan coating composition. This eliminated the need for accurately metering the kappa-carrageenan. During the moulding process the excess was allowed to flow over the top of the can. Immediately after the kappa-carrageenan was introduced, the moulding ram was lowered into the cathode and the kappa-carrageenan coating composition flowed between the outer  
15      surface of the ram and the inner surface of the cathode. After the coating composition solidified, the ram was raised, and the cathode was removed from the ram. Excess kappa-carrageenan material was removed from the area above the cathode shelf. Anode paste was introduced into the cathode having the separator formed directly thereon, and a collector assembly was placed on the can and pressed in place using a small hand  
20      press. The cells were tested for open circuit voltage immediately after fabrication and for a short period thereafter. The cells were put on 71°C shelf-testing and 71°C, 0.8 volts post-partial discharge (PPD) testing. Controls were made by adding anode paste to cathodes lined with conventional paper separators and by pressing collector assemblies in place.

25

One hundred and three (103) operational cells were made with kappa-carrageenan separators. All of the kappa-carrageenan separators were fabricated using the ram moulding technique. These tests proved that operational batteries could be fabricated with separator membranes that are made by applying a coating composition to  
30      the cathode surface and allowing the coating composition to solidify.

Fabrication of Alkaline Cells Having Kappa-Carrageenan/Hydroxyethyl Cellulose Blend Separators

Two master batches were prepared, including a first containing 5 % kappa-carrageenan in water, and a second containing 5 % hydroxyethyl cellulose in water (both on a weight basis). The pH of the hydroxyethyl cellulose batch was increased to 12 by addition of solid potassium hydroxide. The batches were mixed in a ratio of three parts of the composition containing the kappa-carrageenan to one part of the composition containing the hydroxyethyl cellulose. The AA batteries were prepared in accordance with the method described above. Sixty (60) operational cells were made with the 5 kappa-carrageenan/hydroxyethyl cellulose blend separators, and 50 controls were made with conventional paper separators. The open circuit voltages for the batteries containing the kappa-carrageenan/hydroxyethyl cellulose separators were comparable to conventional batteries containing a paper separator. Three (3) of the cells containing the ram moulded kappa-carrageenan/hydroxyethyl cellulose separators lasted 8 weeks with 10 a final average open-circuit voltage reading of 1.236 volts. The remainder of the cells containing the kappa-carrageenan/hydroxyethyl cellulose separators lasted 8 weeks with 15 a final average open-circuit voltage reading of 1.236 volts. The remainder of the cells failed after 2 to 3 weeks. These results demonstrate that alkaline batteries can be successfully prepared with a separator which is formed by applying a coating composition to the cathode surface and allowing the coating composition to solidify.

20 Centrifugally Cast Separators

A kappa-carrageenan/hydroxyethyl cellulose blend as described above was successfully centrifugally cast on the inner surface of a cathode for a cylindrical AA alkaline cell. The AA cells were inserted into a support fixture that was mounted to the output shaft of a DC motor and rotated at approximately 20° to horizontal. The axis of 25 rotation was coincident with the longitudinal axis of the cylindrical cell. The coating composition containing kappa-carrageenan and hydroxyethyl cellulose was introduced into the cathode using a syringe as previously described. The cell was then rapidly accelerated to 2500 rpm and held at that speed for approximately 2 minutes, causing the liquid to flow up the sides of the cathode and to solidify or set-up. In order to avoid complications of measuring the amount of liquid injected into the cell, the cells were 30 overfilled. During the spinning operation, the excess liquid exited from the top of the

cell. After the separators set-up, the cathodes were removed from the spinning fixtures, and additional potassium hydroxide was added. The anode paste was then added along with additional potassium hydroxide, and the collector was installed. Eleven (11) operational cells were produced by the centrifugal casting technique. This test  
5 demonstrated that centrifugal casting can be effectively used for applying a coating composition to a cathode surface to form a separator directly on the cathode surface.

Polyvinyl Acetate Separators

The above centrifugal casting process was repeated using a polyvinyl acetate aqueous dispersion. Three (3) operational cells were made with polyvinyl acetate membranes.  
10

Fabrication Of Cells Using Separator Coating Composition Containing Solid Cellulose Fibres

A master batch of 5 % kappa-carrageenan (weight basis) in water was prepared at 90°C. A master batch of 5 % hydroxyethyl cellulose (by weight) in 1 % potassium hydroxide (by weight) was prepared. The kappa-carrageenan composition and the hydroxyethyl cellulose composition were mixed in a 3:1 ratio at 90°C. To this blend was added 15 % cellulose fibre by weight. Ram moulding, as described above, was  
15 used for preparing AA cells having a separator formed from the coating composition containing kappa-carrageenan/hydroxyethyl cellulose/cellulose fibre. Seventy-seven (77) operational cells were prepared with the kappa-carrageenan/hydroxyethyl cellulose/cellulose fibre blend. Nine of ten batteries subjected to a 71°C shelf test were  
20 operational after 8 weeks, and four of five batteries subjected to a 0.8 volt PPD test were operational.  
25

**CLAIMS**

1. A battery comprising first and second electrodes, an alkaline electrolyte, and an ionically conductive separator disposed between the electrodes, the separator being formed by applying a coating composition to the surface of at least one of the electrodes and solidifying material contained in the coating composition, the coating composition comprising a gel or polymer dispersed in a polar solvent.
- 5
- 10 2. A battery according to claim 1, wherein the coating composition comprises kappa-carrageenan, lambda-carrageenan, iota-carrageenan, hydroxymethyl cellulose, hydroxyethyl cellulose, hydroxypropyl cellulose, or combination thereof, and preferably comprises kappa-carrageenan, hydroxyethyl cellulose, or a blend of kappa-carrageenan and hydroxyethyl cellulose.
- 15
- 15 3. A battery according to claim 2, wherein the coating composition comprises from about 1 to about 10 weight percent kappa-carrageenan.
- 20 4. A battery according to claim 1, wherein the coating composition comprises a synthetic polymer.
- 25 5. A battery according to claim 4, wherein the synthetic polymer is polyvinyl acetate.
6. A battery according to claim 4, wherein the synthetic polymer comprises polyurethane, acrylic polymer, epoxy polymer, or a combination thereof.
7. A battery according to claim 1, wherein the coating composition comprises cellulose viscose.

8. A battery according to any preceding claim, wherein the coating composition includes fibres, preferably fibres selected from cellulose, cotton, rayon, boron, boron carbide, boron nitride, aluminium silicate, fused silica fibres, wood pulp, and polyolefin fibres.

5

9. A battery according to any preceding claim, wherein the coating composition includes a cross-linking agent, preferably divinylsulphone or trishydroxymethyl cyanurate.

10 10. A battery according to any preceding claim, wherein the separator occupies less than 10% of the volume of the battery.

11. A battery according to any preceding claim, wherein the separator has a solvent content greater than 50% by weight.

15

12. A battery according to any preceding claim, wherein the separator has controlled variation in thickness.

13. A battery according to any preceding claim, wherein the separator has sufficient elasticity to sustain at least 25 % expansion of the cathode dimensions during discharge.

14. A battery according to any preceding claim, wherein the coating composition is a polymer blend comprising at least two different polymers.

25 15. A battery according to claim 1, wherein the coating composition comprises a thermoplastic gel, preferably a thermoplastic gel having a melting point greater than 71°C.

30 16. A battery according to any preceding claim, wherein the material in the coating composition is solidified by drying, curing, gelling, cross-linking, polymerisation, freezing, or a combination of these techniques.

17. A method of providing a separator on an electrode for an alkaline battery, comprising:

5 applying a liquid aqueous coating composition to an electrode surface; and  
solidifying the coating composition on said electrode surface to form a separator  
membrane.

18. A method according to claim 17, wherein the coating composition is applied by introducing the coating composition into the bottom of a cathode and introducing a  
10 forming ram into the cathode to form an annular space between the interior surface of the cathode and the outer surface of the ram and to cause the coating composition to flow up into said annular space, solidifying the coating composition and removing the ram from the cathode.

15 19. A method according to claim 17, wherein the coating composition is applied to the cathode surface by introducing a ram having a coating composition outlet port into the cathode, introducing the coating composition into the cell through the port, causing the separator material to flow into an annular space between the ram and the inner surface of the cathode, solidifying the coating composition and removing the ram from  
20 the cathode.

20. A method according to claim 17, wherein the coating composition is applied to the surface of a cathode by centrifugal casting, preferably by introducing the coating composition into a cathode cup disposed in a cylindrical can and rotating the cylindrical  
25 can at a high speed to cause the coating composition to flow along the internal surface of the cathode cup and solidify, the axis of rotation being coincident with the longitudinal axis of the cylindrical can, the axis of rotation of the cylindrical can in which the cathode is disposed being at an angle between and including a vertical axis and a horizontal axis.

21. A method according to claim 17, wherein the coating composition is applied by spraying.
22. A method according to any of claims 17 to 21, wherein the coating composition  
5 is a gel or polymeric dispersion.
23. A method according to any of claims 17 to 22, wherein the coating composition comprises kappa-carrageenan, lambda-carrageenan, iota-carrageenan, hydroxymethyl cellulose, hydroxyethyl cellulose, hydroxypropyl cellulose, or a combination thereof,  
10 and preferably comprises kappa-carrageenan, hydroxyethyl cellulose, or a combination of kappa-carrageenan and hydroxyethyl cellulose.
24. A method according to any of claims 17 to 22, wherein the coating composition  
comprises a synthetic polymer.  
15
25. A method according to claim 24, wherein the synthetic polymer is polyvinyl acetate.
26. A method according to claim 24, wherein the synthetic polymer is polyurethane,  
20 acrylic polymer, epoxy polymer, or a combination thereof.
27. A method according to any of claims 17 to 22, wherein the coating composition  
comprises cellulose viscose.
- 25 28. A method according to any of claims 17 to 27, wherein the coating composition includes fibres selected from cellulose, wool, silk, cotton, rayon, boron, boron carbide, boron nitride, carbon, aluminium silicate, fused silica fibres, wood pulp and polyolefin  
fibres.
- 30 29. A method according to any of claims 17 to 28 further comprising a cross-linking agent, preferably divinylsulphone or trishydroxymethyl cyanurate.

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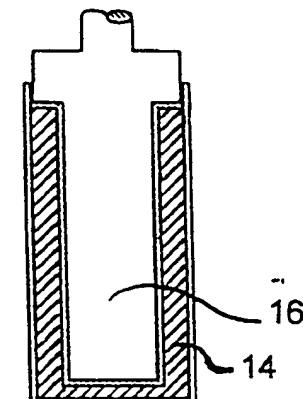
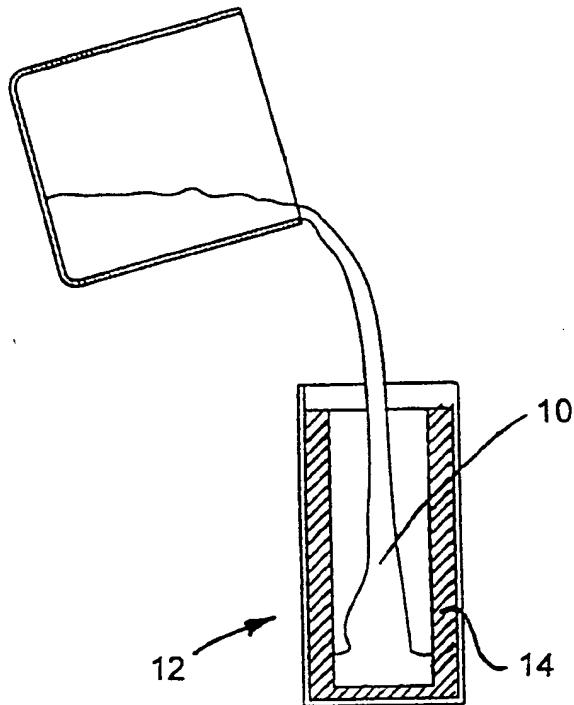


Fig. 2

Fig. 1

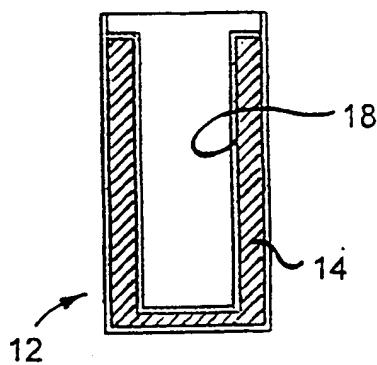


Fig. 3

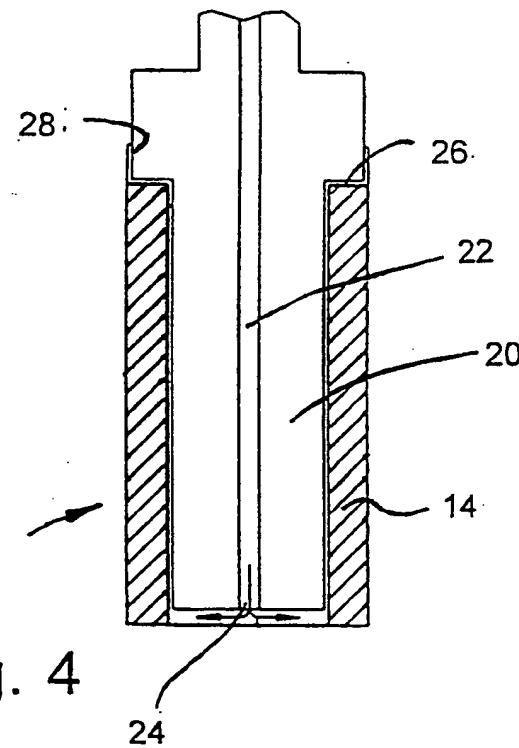


Fig. 4

# INTERNATIONAL SEARCH REPORT

International Application No  
PCT/US 99/30275

**A. CLASSIFICATION OF SUBJECT MATTER**  
 IPC 7 H01M2/16 H01M6/04 H01M10/24

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
 IPC 7 H01M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 3 892 594 A (CHARLESBY ARTHUR ET AL) 1 July 1975 (1975-07-01)  example 2	1,4-6, 16,17, 24-26
X	US 5 837 015 A (MOORE JOHN ET AL) 17 November 1998 (1998-11-17) column 5, line 6-58  example 3	17,24-26
X	EP 0 814 520 A (IMRA AMERICA INC) 29 December 1997 (1997-12-29) column 5, line 5-36 column 7, line 54-58  examples	1,4-6
Y		17,24-26
		-/-

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

\* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
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- "&" document member of the same patent family

Date of the actual completion of the international search

5 May 2000

Date of mailing of the international search report

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Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl.  
Fax: (+31-70) 340-3016

Authorized officer

Engl, H

## INTERNATIONAL SEARCH REPORT

Intell. 1al Application No  
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## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

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Y	_____	17,24-26
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